

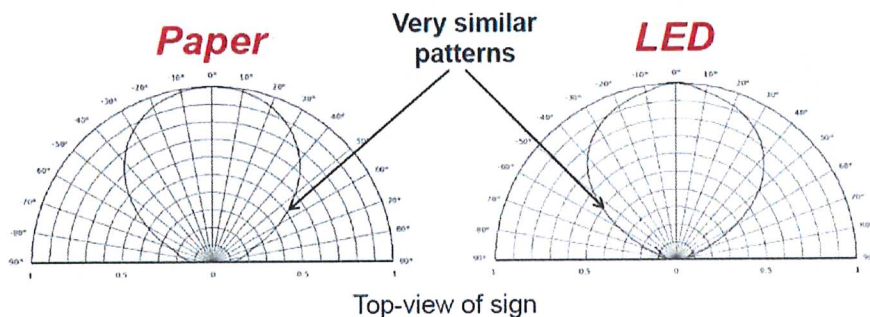
McHenry County Department of Planning & Development

RE: Digital Viewing Cone specifics- Vertical and Horizontal v6

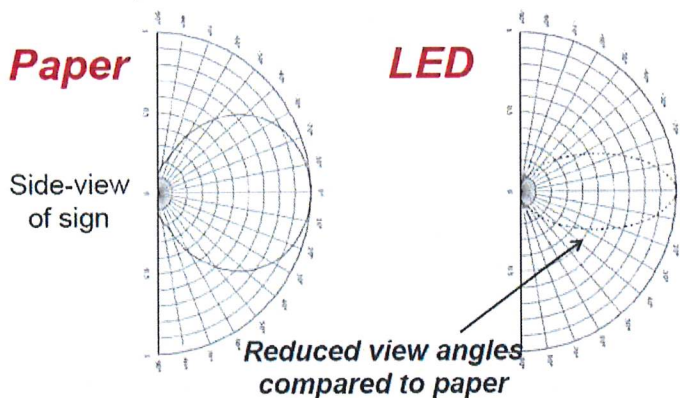
The technological specifics of LED lighting are unique. Our signs will not contribute to the overall sky glow for three main reasons:

- 1 The LED's used in our signs have diodes focusing the emitted light into a directed beam.
  - 2 The signs are aimed at the roadway so vehicular traffic can easily see the advertising message.
  - 3 Horizontal Louvers manufactured as part of the sign face help to prevent upward illumination.
- The first chart below is to be viewed as if the horizontal line at the bottom is the billboard face, viewed from overhead. This displays how the illuminance continues to reduce as you get more parallel to the sign face. Gradually reducing to nothing. If you stand right next to the sign, no light is visible. If you stand directly beneath the sign, no light is visible on the ground immediately around you.

Light from the LED sign face is spread horizontally and vertically.  
Horizontally:



And Vertically:



-Source: Nichia Specifications for Blue LED <http://www.nichia.com/specification/en/product/led/NSPB346KS-E.pdf>

### Myth:

Digital billboards produce large amounts of sky glow.

### The Facts:

Sky glow results from the use of lighting fixtures that emit light above a horizontal plane so that it enters the atmosphere directly. Digital billboards contain directional LEDs that prevent sky glow which may be produced by traditional billboards.

Fluorescent and standard 'bulb' shaped incandescent lamps emit light in all directions. This leads to a large portion of the light produced by the lamp escaping from the fixture in a direction that is not useful for the intended application, specifically above the sign. Digital billboards' directional LEDs, however, prevent excess light spillage in unintended locations. Additionally, louvers on these signs assist in controlling the light output by shielding any light directed upward.

### DAKTRONICS

Daktronics specs a 70-degree vertical and a 140-degree horizontal viewing angle for their displays.

### WATCHFIRE

Yesco specs a 70-degree vertical and a 140-degree horizontal viewing angle for their displays.

### FORMETCO

Yesco specs a 60-degree vertical and a 140-degree horizontal viewing angle for their displays.

### MEDIA RESOURCES

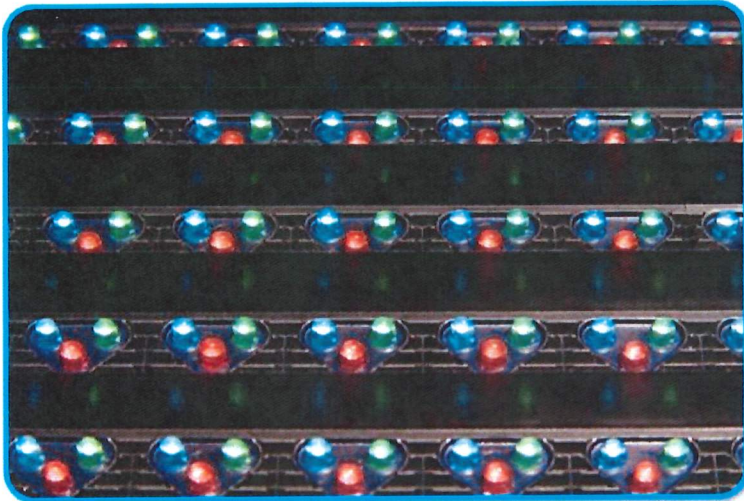
Yesco specs a 70-degree vertical and a 140-degree horizontal viewing angle for their displays

### YESCO

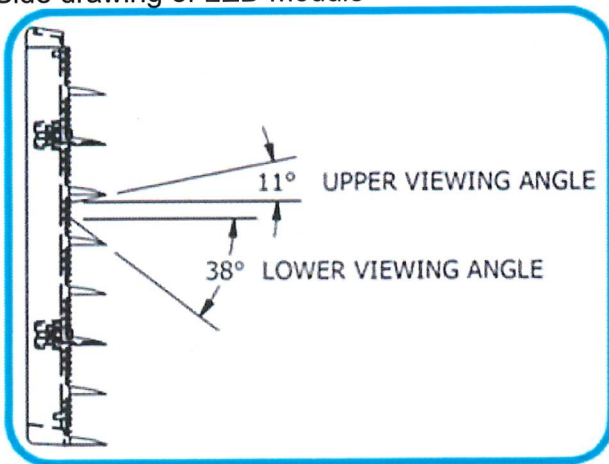
Yesco specs a 49-degree vertical and a 120-degree horizontal viewing angle for their displays.

Light from the LED sign face is spread horizontally and vertically. This is also demonstrated by side view drawings showing how the louvers decrease sky glow.

Close up of LED module horizontal louvers:



Side drawing of LED module



**-Source Yesco**

The illuminance of the area around the sign is not uniform. The illuminance is greatest in the area that is directly perpendicular to the sign, and gradually tapers off to nothing as you become more directly parallel to the sign. This result is because a LED sign is not a uniform light source, but rather it focuses the light in specific directions. For this reason, the brightest point is directly perpendicular to the sign, and gradually fades out as you move outside the viewing cone of the sign.

During daylight conditions, the illuminance area reaches as far as 250 feet from the sign at 0 degrees from center. During nighttime conditions, the illuminance area reaches a maximum of 100 feet from the sign at 0 degrees from center. This scenario contemplates signs at ground level. These distances will decrease further when you factor in that the bottom of the sign face is 33 feet in the air. Just as the horizontal viewing angle affects how much area the sign illuminates, the vertical height of the sign also affects how much area the sign illuminates.

McHenry County Department of Planning & Development

RE: Digital impact on Ambient Light

There are 3 necessary components to ensure a digital billboard will never be too bright for conditions.

- 1 An ambient light sensor installed on the sign structure.
- 2 Dimming software
- 3 Maximum brightness limits incorporating a footcandle standard.

The ambient light level of a CCO digital billboard will not vary significantly from that of a traditional billboard display. (In many cases it will be less.) We will set the light levels to be appropriate for the surroundings.

We utilize a photocell on all our digital billboards so that the display will easily be seen by motorists under changing light conditions. Sophisticated dimming software constantly changes the brightness of the display in response to changing ambient lighting conditions. This insures a CCO digital billboard will never be too bright for conditions.

The range of brightness varies greatly between daytime and nighttime conditions. In bright daylight, the unit must have higher intensity in order to be seen. During darkness conditions, the brightness can be set low and still be easily seen by motorists.

### **Lighting Standards – Measurements:**

The industry recommended criteria follow the lighting standards established by the Illuminating Engineering Society of North America (IESNA). All OAAA member companies are already operating their digital signs according to these lighting criteria.

Recommended regulatory criteria:

Lighting levels will not increase by more than 0.3-foot candles (over ambient levels) as measured using a foot candle meter at a pre-set distance.

Each display must have a light sensing device that will adjust the brightness as ambient light conditions change.

Pre-set distances to measure the foot candles impact vary with the expected viewing distances of each size sign. Measurements should be taken as close to perpendicular to the face as practical.

Measurement distance criteria:

Nominal Face Size	Distance to measure from
12' x 24'	150'
10'6" x 36'	200'
14' x 48'	250'
20' x 60'	350'

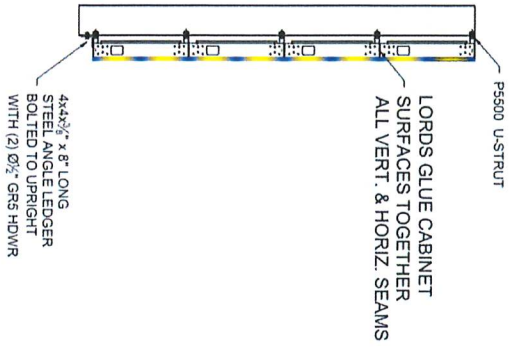
Each display will have a light sensing device that will adjust the brightness as ambient light conditions change. We can set the photometrics from the manufacturer to consistently meet the above target day or night.

# PRODUCT SPECS

Specification	Formetco Standard Poster Unit	Formetco LCLW Poster Unit
<b>Weight (Based on 12 X 24) Poster</b>	3,000 LBS	1,400 LBS
<b>Panel Size</b>	10' 6" X 24' 1.75"	10' 6" X 22' 3"
<b>Pixel Matrix</b>	200 H x 460 W	*192 H x 408 W
<b>Power Supply</b>	5.19 AMPS	4.52 AMPS
<b>Resolution</b>	16MM	16.6MM
<b>Module Count</b>	230	136
<b>Service</b>	Rear/Front Service	Rear/Front Service
<b>Brightness Guarantee</b>	7500 NITS Shipped (Up to 10,000 NITS capable)	7500 NITS Shipped (Up to 10,000 NITS capable)
<b>Web Camera</b>	Included Mobotix M26	Included Mobotix M26
<b>Warranty Coverage</b>	10-Year all Components, 1-Year covered labor	10-Year components, *7-Year Modules, 1-Year covered labor

\*Still meets aspect ratio

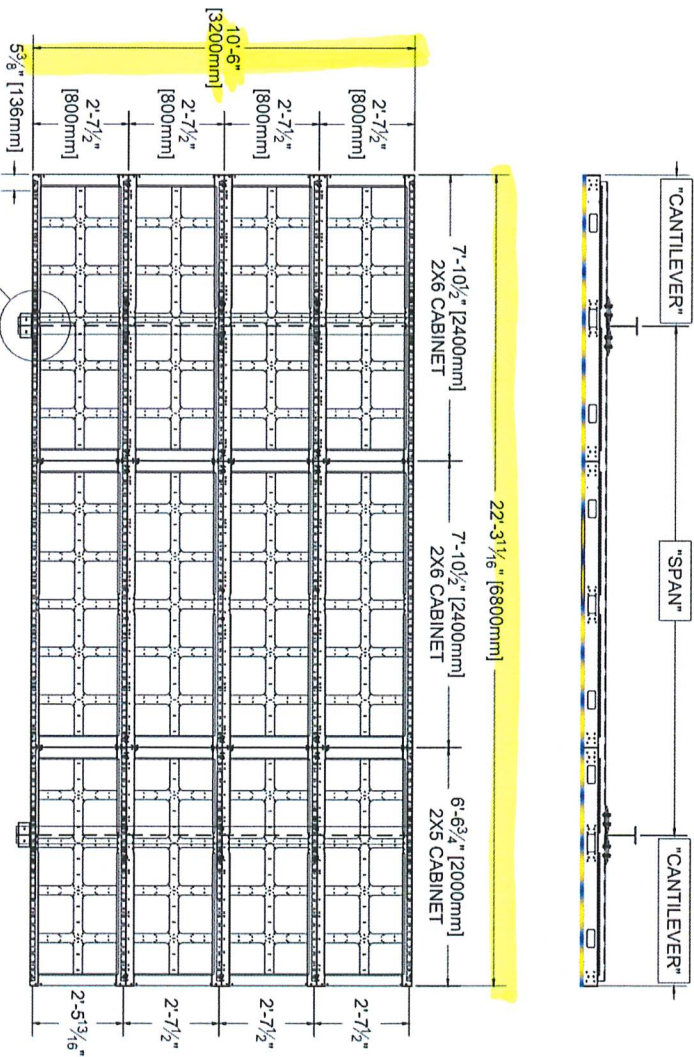
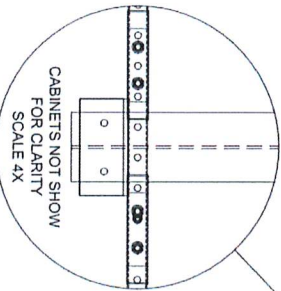
Maximum Pressure for Upright Spacing (est. by SolidWorks modeling-Case A)			
Upright Spacing	Cantilever	Span	Max Pressure
10.50	ft	5.90	32 psf
12.00	ft	5.15	45 psf
14.00	ft	4.15	40 psf
16.00	ft	3.15	28 psf



ESTIMATED BASE ASSEMBLY WEIGHT TWO UPRIGHTS @ VARIOUS CENTERS

HORIZONTAL FLT CABINETS, MOUNTING U-STRUT/CLAMPS/HDWR, CONNECTORS AND LEDGERS SUPPLEMENTAL STEEL.

TOTAL 1833#



U-STRUT MOUNTING CONFIGURATION (5) P5500 Unistrut (or equivalent) @ top and bottom and each cabinet joint

NOT FOR PERMIT

**FORMETCO**

REV	DESCRIPTION	DATE	APPD	REV	DATE	REV	DATE	REV	DATE
C	UPDATE MOUNTING AND WEIGHT (est. SOLIDWORKS)	9-9-22	RFV	9-9-22	RFV	9-9-22	RFV	9-9-22	RFV
B	UPDATE MOUNTING AND WEIGHT	8-31-22	RFV	8-31-22	RFV	8-31-22	RFV	8-31-22	RFV
A	UPDATE WEIGHT	8-29-22	RFV	8-29-22	RFV	8-29-22	RFV	8-29-22	RFV

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NO NOT SCALE THIS DRAWING

SCALE 1/4" = 1'-0"

DATE 07-20-22

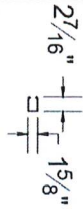
BY JVC

APPD H-H-22

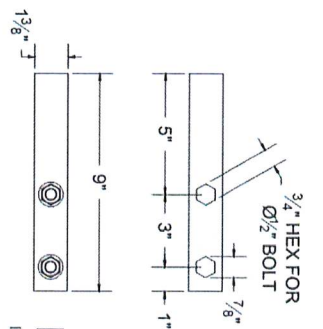
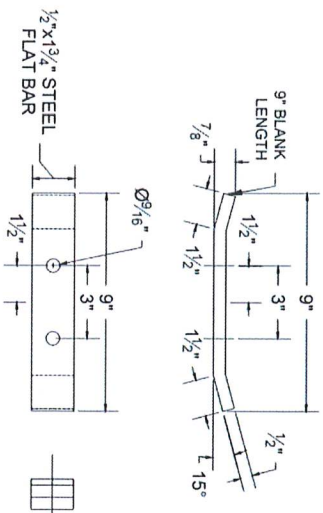
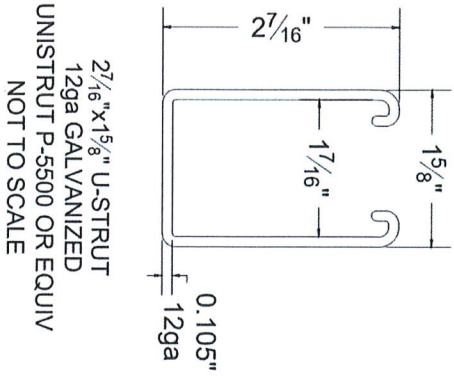
2963 Pleasant Hill Rd. Duluth, GA 30096-3808

1667mm FLT 192x408 LT WT POSTER

U-STRUT MOUNTING I-BEAM CLAMPS



U-STRUT 2-7/16"x1-5/8"  
 MAKE 5



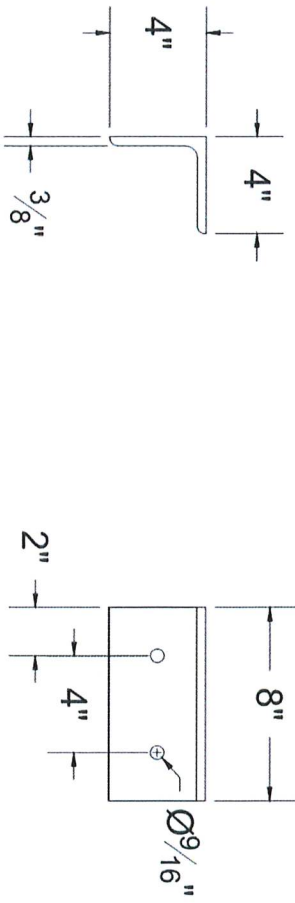
FORMED I-BEAM CLAMP  
 SINGLE WIDTH  
 1-3/4"x1/2" FLAT BAR  
 PAINT GRAY  
 SCALE 4X  
 QTY = 20 REQ'D

U-STRUT CLAMP BOLT PLATE  
 1-3/75" x 9" FLAT  
 12ga GALVANNEAL  
 SCALE 4X  
 QTY = 20 REQ'D

NOTE: PAINT GRAY  
 UPRIGHT BEAM CLAMP - 1/2" THICK

REV	DESCRIPTION	DATE	APP'D	PART NUMBER	2963 Pleasant Hill Rd. Duluth, GA 30096-3808
1	REVISIONS			LT WT POSTER	
	THIS MATERIAL IS THE EXCLUSIVE CONFIDENTIAL PROPERTY OF FORMETCO, INC.				
	ALL RIGHTS, INCLUDING COPYRIGHT AND PATENT RIGHTS, ARE RESERVED BY FORMETCO, INC.				
	DO NOT COPY THIS DRAWING WITHOUT PERMISSION OF FORMETCO, INC.				
	APPROVALS	DATE	APP'D	SCALE	1:40
	BY: [Signature]	07-2022	[Signature]	SH 2	
	DATE	11-11-22			
	DESCRIPTION	U-STRUT MOUNTING I-BEAM CLAMPS			





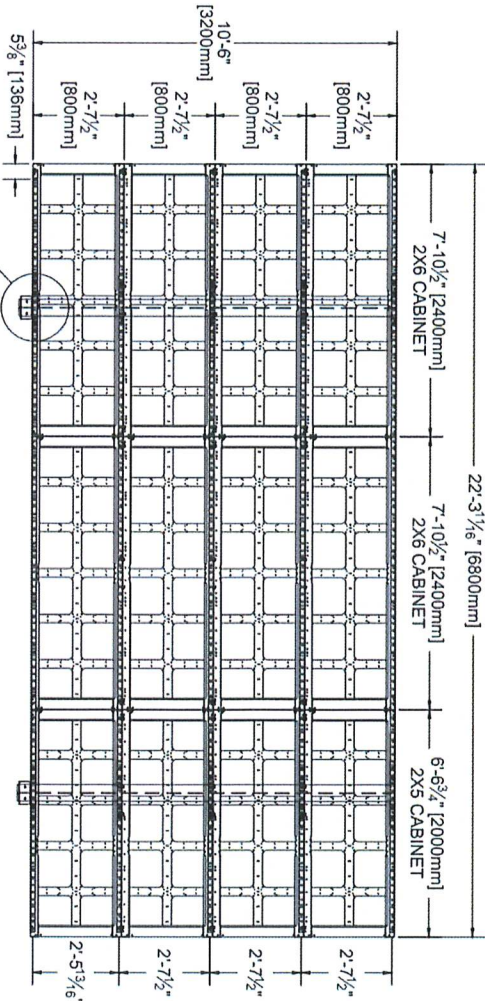
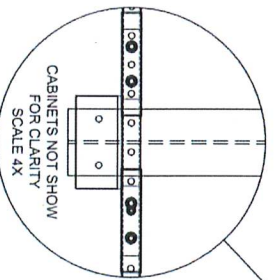
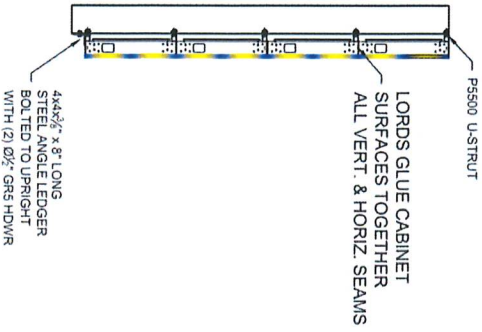
4X4X3/8" X 8" LONG  
 STEEL ANGLE LEDGER  
 REQUIRES 2 PER DISPLAY  
 PAINT BLACK

P/N: XXXXXXXXXXXXXXXX  
 CUT 30 PIECES FROM  
 4X4X3/8" STEEL ANGLE  
 X 20' LONG STOCK  
 PAINT BLACK

REV	DESCRIPTION	DATE	APPD	PART NUMBER	2963 Pleasant Hill Rd. Duluth, GA 30096-3808
	REVISIONS			8X17 WT POSTER	FORMETCO
				APPROVALS	
				REVISED	1667mm FLT 192x408 LT WT POSTER
				DATE	LEDGER FABRICATION
				11-14-22	
				DO NOT SCALE	SCALE 1:40
				THIS DRAWING	DRG B-3540
				DO NOT COPY THIS DRAWING WITHOUT PERMISSION OF FORMETCO, INC.	SH 3



Maximum Pressure for Upright Spacing (est. by SolidWorks modeling-Case A)			
Upright Spacing	Cantilever Span	Pressure	Max
10.50	ft	5.90	32 psf
12.00	ft	5.15	45 psf
14.00	ft	4.15	40 psf
16.00	ft	3.15	28 psf



**MOUNTING CONFIGURATION**  
 (5) P5500 Unistrut (or equivalent)  
 @ top and bottom & each cabinet joint

ESTIMATED BASE ASSEMBLY WEIGHT  
 TWO UPRIGHTS @ VARIOUS CENTERS

HORIZONTAL FLT CABINETS,  
 MOUNTING U-STRUT/CLAMPS/HDWR,  
 CONNECTORS AND LEDGERS  
 SUPPLEMENTAL STEEL.

1481.2#  
 317.2#  
 34.4#  
 0.0#  
 1833#

REV	DESCRIPTION	DATE	APPD	REV	DESCRIPTION	DATE	APPD
C	UPDATE MOUNTING AND WEIGHT (est. SOLIDWORKS)	9-9-22	RFV				
B	UPDATE MOUNTING AND WEIGHT	8-31-22	RFV				
A	UPDATE WEIGHT	8-29-22	RFV				

REV	DESCRIPTION	DATE	APPD
1	ISSUED	9-9-22	RFV
2	REVISED	9-9-22	RFV

REV	DESCRIPTION	DATE	APPD
1	ISSUED	9-9-22	RFV
2	REVISED	9-9-22	RFV

**FORMETCO**  
 2963 Pleasant Hill Rd. Duluth, GA 30096-3908

8x17 LIGHT WEIGHT LED POSTER  
 MOUNTING CONCEPT I-BEAM CLAMPS

NO NOT SCALE THIS DRAWING

SCALE: 1:40

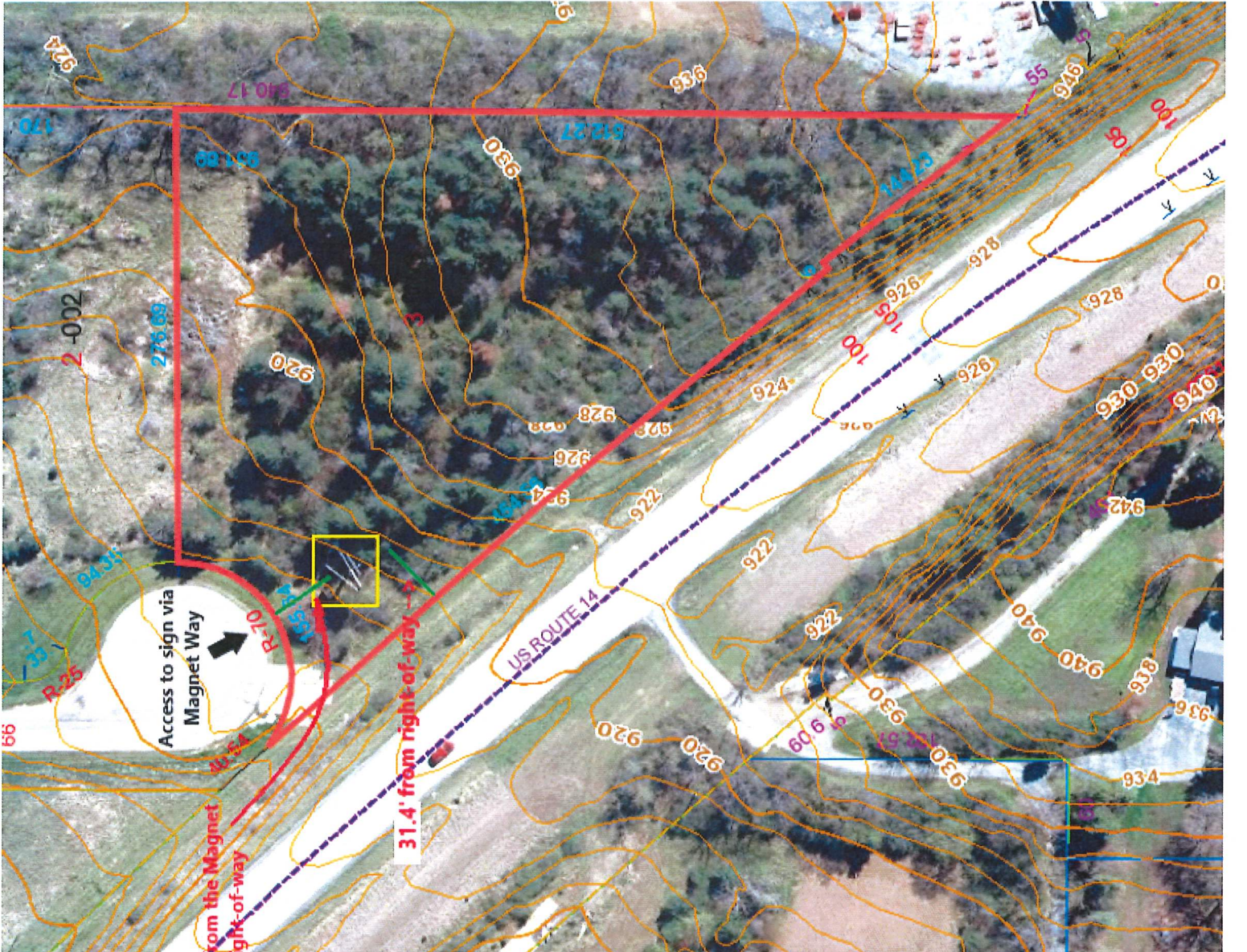
SH 1 OF 1

**NOT FOR PERMIT**





Lighting levels will not increase by more than 0.3 foot candles (over ambient levels) as measured using a foot-candle meter at a pre-set distance, in accordance with State and Federal regulations and as set forth by the Outdoor Advertising Association of America (OAAA).



**PARCEL DETAILS**

PIN:  [Get Details](#)

Year: 2023 - Payable 2024

DETAILS TAX INFO MISC DOCUMENTS

**LEGAL DESCRIPTION**

DOC 2007R0083528 (RE-RECORD)  
 LT 3 ARNOLD SUB MEMO RT 14 DEDICATED PER DOCS  
 368978 & 343730

**SALES**

Date of Sale Amount

**LOT ACRES**

Lot Size Homesite Farm Gross Acres





7264 W Benton Dr, Frankfort, IL 60423  
(815) 595-VOSS (8677)

CLIENT CLEAR CHANNEL  
VOSS NO. 23-017-574  
JOB 25-3786  
DATE 3/28/2024 ENG. WY 1/16

IL FIRM NO 184-008800

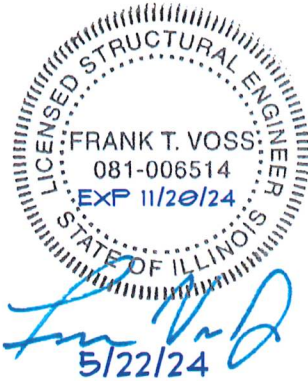
LOCATION: RT 14, 0.6 MI E/O RT 320 NS  
WOODSTOCK, IL

BUILDING CODE: 2018 INTERNATIONAL BUILDING CODE

WIND: 100 MPH, EXP "C," IW = 1  
PER ASCE 7-16  
RISK CATEGORY I PW = 20.8 PSF

SEISMIC:  $S_s = 0.108 g$   $S_1 = 0.058 g$   
 $S_{DS} = 0.116$   $S_{D1} = 0.093$   
SC = D, SDC = B, CS = 0.039, V = CS\*W = 0.50K

DESCRIPTION: ADD 2 DIGITAL FACES TO EXISTING  
BILLBOARD STRUCTURE



EX: 12X24.5, CM, 10' NOM V, 42' OAH  
PROP: 10.5'X22.33', CM, 10' NOM V, 42' OAH

DESIGNED FOR INSTALLATION OF  
ONE OR TWO STRINGERLESS HEAVY  
FACES WEIGHING UP TO 1800# EACH

DocuSigned by: 5/22/2024  
Frank Voss  
08A61EA841854CE...

FRONT WALKS NOT TO BE REMOVED  
- NEEDED FOR ACCESS

NO REAR WALKS EXCEPT ACCESS WALK  
FROM COLUMN TO WALKAROUND

This drawing has been digitally signed  
and sealed by Frank Voss on the date  
adjacent to the seal.  
Printed copies of this document are  
not considered signed and sealed,  
and the signature must be verified  
on any electronic copies.



CLIENT CLEAR CHANNEL  
 VOSS NO. 23-017-574  
 JOB 25-3786, Ex.  
 DATE 3/28/2024 ENG. FV

2/16

**Load Comparison of alterations to existing billboard structure**

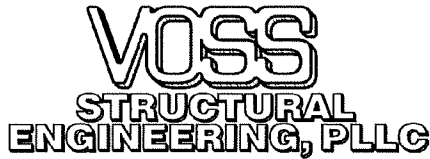
Building Code assumed at time of original construction: 2003 International Building Code  
 Current Building Code for new structures: 2018 International Building Code  
 Existing Building Code: 2018 Existing Building Code

Comparison using Code for New Structures as basis

	2018 IBC Loading				
	Existing	Proposed		Proposed	
		1 LED	% increase	2 LED	% increase
Overall height	42	42		42	
Sign height (H)	12	12		12	
Sign width (W)	24.5	24.5		24.5	
Apron + extra	0.75	0.75		0.75	
Flag	0	0		0	
Offset (incl. face wt.)	0.2808196	0.55		0.27	
Head weight	7.16	8.63		9.29	
Natural frequency (f)	1.412	1.302		1.260	
Gust effect factor (G, Gf)	0.850	0.850		0.850	
Wind pressure (pw)	20.8	20.8		20.8	
Column 1 Fy	35	35		35	
Column 1 IC	0.959	0.974	1.62%	0.968	1.01%
Torsion Fy	35	35		35	
Torsion IC	3.062	3.218	5.11%	3.193	4.30%
Foundation Depth	15.0	15.0		15.0	
Foundation IC	1.008	1.018	1.02%	1.013	0.48%

Loads on column and foundation are not increased more than 5% by this alteration, need not upgrade to meet new code for new structures.

Torsion pipe is significantly overstressed, provide reinforcement to torsion pipe to reduce stress due to proposed and future loads.



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(815) 595-VOSS (8677)

CLIENT CLEAR CHANNEL  
 VOSS NO. 23-017-574  
 JOB 25-3786  
 DATE 3/28/2024 ENG. WY

3/16

**Overall Data Sheet**

Location: Rt 14, 0.6 mi E/O Rt 320 NS, Woodstock, IL

Building Code: 2018 International Building Code

Wind Code: ASCE 7-16

Wind Speed (V): 100 mph 3 Second Gust ASIF = 1

Wind Exposure: C

Wind Importance ( $I_w$ ): 1.00

Max Overall Height: 42.0 ft

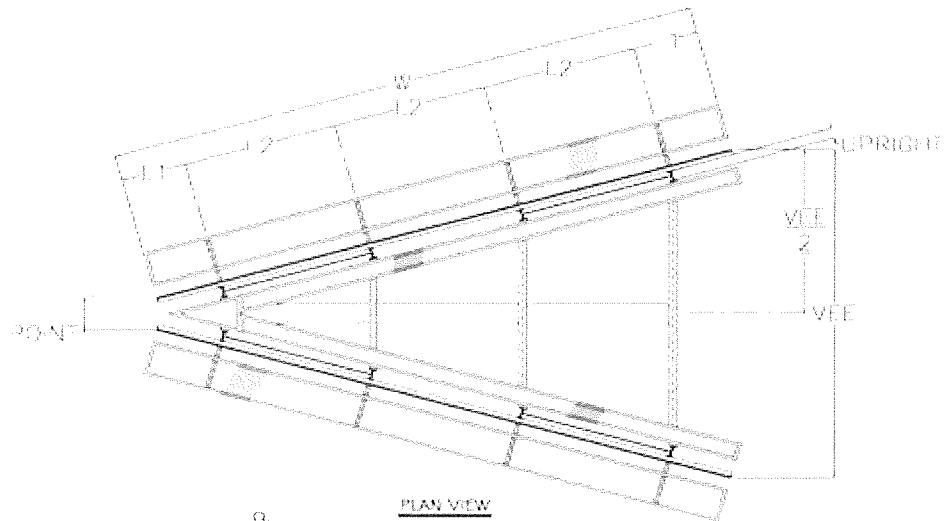
Sign Height (H): 12.0 ft

Sign Width (W): 24.5 ft

Apron plus extra: .75 ft

Flag (CL face to CL column) .0 ft

Offset (CL torsion pipe to CL Column) .0 ft



**Superstructure Layout**

Cantilever (L1) 4.25 ft

Upright Spacing (L2) 16.0 ft

Point width (Point) 6.0 ft

Vee width (Vee) 11.0 ft

Upright (Upright) 30.0 in

Number of Uprights 2

Spreader 11.5 ft

Torsion Pipe 11.5 ft

Catwalk location (Cat) 3.75 ft

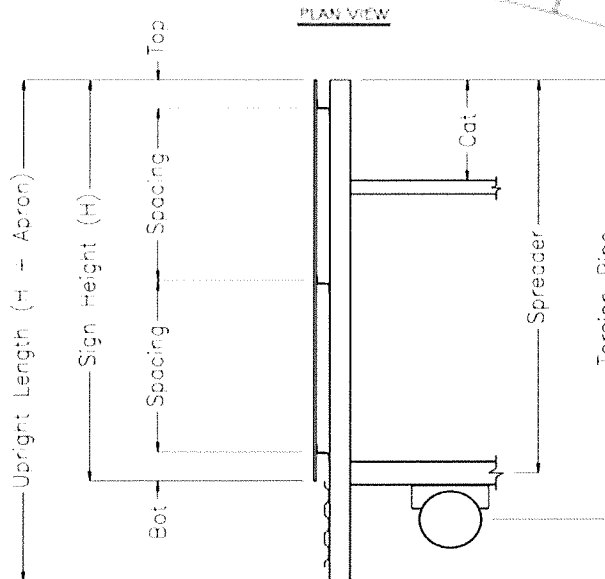
Top Stringer (Top) .75 ft

Bot Stringer (Bot) .25 ft

Number of stringers 3

Stringer Spacing (Spacing) 5.5 ft

Lat br spacing 11.0 ft



**Various Other Data**

Wall Thickness factor 0.93

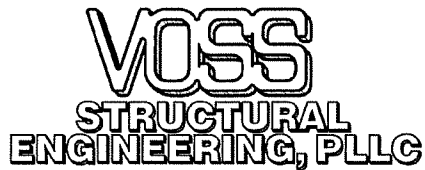
Poff Multiplier 1

Xbracing locations

Bay1

X





7264 W Benton Dr, Frankfort, IL 60423  
(815) 595-VOSS (8677)

CLIENT CLEAR CHANNEL  
 VOSS NO. 23-017-574  
 JOB 25-3786  
 DATE 3/28/2024 ENG. WY 4/16

### Seismic Design Criteria

Building Code: 2018 International Building Code  
 Subsection: 1603.1.5 - Earthquake Design Data  
 ASCE Std: ASCE 7-16

1. Seismic importance Factor:  $I_E = 1.00$   
 Risk Category (Table 1604.5): **I**

2. Mapped Spectral Response accelerations (From USGS Website):  
 Lat: 42.3331  $S_S = 0.108$  g  
 Long: -88.4782  $S_1 = 0.058$  g

3. Site Class: **D**

4. Spectral Response Coefficients:

$S_{DS}$	<b>0.116</b>	$f_v$	<b>2.400</b>	2.4
$S_{D1}$	<b>0.093</b>	$f_a$	<b>1.600</b>	1.6

5. Seismic Design Category: **B**  
 $S_{DS} S_{DC}$  A  
 $S_{D1} S_{DC}$  B

6. Basic Seismic Force Resisting System:  
**Non-Building Structures Not Similar to Buildings - Signs and Billboards**

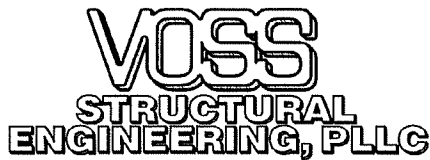
7. Design Base Shear:  $V = C_s * W = 0.50$  kips Wind Governs over Seismic

8. Seismic Response Coefficient,  $C_s = 0.039$

9. Response Modification Factor (ASCE 7-16, Table 15.4-2)  
 $R = 3$

10. Analysis Procedure Used: **Equivalent Lateral Force Method**





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 JOB 25-3786  
 DATE 3/28/2024 ENG. WY

6/16

**Wind Design Data**

Building Code: 2018 International Building Code  
 Wind Code: ASCE 7-16  
 Wind Speed (V): 100 mph 3 Second Gust  $V_{ASD}$  77 mph  
 Wind Exposure: C  
 Wind Importance ( $I_w$ ): 1  
 Max Overall Height: 42.0 ft

**Coefficients**

Kz 1.054355 G 0.85  
 Kzt 1 Cf 1.780153  
 Kd 0.85  $\omega$  1  
 LF 0.6

**Load Cases to check**

Load Case 1: Wind load applied at centroid of Sign area  
 Load Case 2: Wind load at 0.2\*Sign Width from Centroid of Sign area  
 Figure 29.3-1, Footnote 3  
 Load Case 3: Case C Computed elsewhere

qs = 22.94 psf  
 pw = 20.83 psf  
 $\omega$  pw = 20.8 psf

Therefore, use **20.83 psf** for design  
 with **1.00 ASIF** (Allowable Stress Increase Factor)  
 (Ultimate pw = 34.7 psf)

Wind applied to computer model with torsion pipe along global X axis:

Wind Pressure perpendicular to sign Face

Sign face angle from Global X-Axis: 5.86 degrees  
 pz 20.7 psf  
 px 2.1 psf

Wind pressure, 60% perpendicular, 30% transverse (used sometimes to size crossbracing)

pz 13.1 psf  
 px 7.5 psf



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7/16

**ASCE 7-05/ASCE 7-10/ASCE 7-16/ASCE 7-22 Wind Pressure Calculations**

V, mph	100				
OAH, ft	42				
Exp	C				
Kz	1.054355				
Kzt	1				
Importance Fa	1				
	1.00				
Kd	0.85				
G	0.85				
Cf	1.780153	s/h	0.303571	0.303571	0.303571
ω	1	B/s	1.921569	1.921569	1.921569
LF	0.6	Cf	1.780153		
q	22.94277	Cf(rounded to nearest)		1	1.8
Design	20.82924				
Pressure	20.82924				

Supporting Tables and Calculations

Table 6-2 - Terrain Exposure Constants

Exposure	α	z <sub>g</sub> (ft)	a	b hat	alpha bar	b bar	c	z <sub>0</sub> (ft)	eps bar	z min (ft)
B	7	1200	0.142857	0.84	0.25	0.45	0.3	320	0.333333	30
C	9.5	900	0.105263	1	0.153846	0.65	0.2	500	0.2	15
D	11.5	700	0.086957	1.07	0.111111	0.8	0.15	650	0.125	7

8.5

Cf, Case A and Case B												
Clearance Ratio, s/h	Aspect Ratio, B/s											
	<0.05	0.1	0.2	0.5	1	2	4	5	10	20	30	>45
1	1.8	1.7	1.65	1.55	1.45	1.4	1.35	1.35	1.3	1.3	1.3	1.3
0.9	1.85	1.75	1.7	1.6	1.55	1.5	1.45	1.45	1.4	1.4	1.4	1.4
0.7	1.9	1.85	1.75	1.7	1.65	1.6	1.6	1.55	1.55	1.55	1.55	1.55
0.5	1.95	1.85	1.8	1.75	1.75	1.7	1.7	1.7	1.7	1.7	1.7	1.75
0.3	1.95	1.9	1.85	1.8	1.8	1.8	1.8	1.8	1.8	1.85	1.85	1.85
0.2	1.95	1.9	1.85	1.8	1.8	1.8	1.8	1.8	1.85	1.9	1.9	1.95
<.16	1.95	1.9	1.85	1.85	1.8	1.8	1.85	1.85	1.85	1.9	1.9	1.95

Cf, Case C														
Region	Aspect Ratio, B/s											Region	13	>45
	2	3	4	5	6	7	8	9	10	10	13			
0 to s	2.25	2.6	2.9	3.1	3.3	3.4	3.55	3.65	3.75	3.75	0 to s	4	4.3	
s to 2s	1.5	1.7	1.9	2	2.15	2.25	2.3	2.35	2.45	2.45	s to 2s	2.6	2.55	
2s to 3s		1.15	1.3	1.45	1.55	1.65	1.7	1.7	1.85	1.85	2s to 3s	2	1.95	
3s to 10s			1.1	1.05	1.05	1.05	1.05	1.05	0.95	0.95	3s to 4s	1.5	1.85	
											4s to 5s	1.35	1.85	
											5s to 10s	0.9	1.1	
											>10s	0.55	0.55	

Case C wind pressures

Region	Cf	pw
0 to s	0.000	0.00
s to 2s	0.000	0.00
2s to 3s	0.000	0.00
3s to 10s	0.000	0.00

Case B vs Case C

	P <sub>max</sub>	P <sub>total</sub>
B	34.78 psf	6.51 kips
C	0.00 psf	0.00 kips
Case B Governs		Case B Governs
#DIV/0!		

Ecc Factor
0.2
#VALUE!
Design Ecc
0.2



CLIENT CLEAR CHANNEL  
 VOSS NO. 23-017-574  
 JOB 25-3786  
 DATE 3/28/2024 ENG. WY

8/16

**Detailed Deadload Takeoff**

**One Heavy Face**

**Side 1**

	Number	Load	Area/Length	Total	Loc.	Mom.
Face	1	8	234.465	1876	4.25	8.0
Stringers	0	5.8	24.5	0	3.41	0.0
Clips	2	6.6	0.75	10	3.41	0.0
Uprights	2	9	12.75	230	3.00	0.7
Hangrail/lat brace	1	4.9	24.5	120	3.00	0.4
Front CW ledgers	2	6.7	5.70	76	6.09	0.5
Ledger Clips	4	4.9	0.42	8	3.00	0.0
Front CW stringers	2	5.8	34.17	396	6.09	2.4
Front CW grating	1	3	87.2	262	6.09	1.6
Apron	0	3	6.125	0	3.00	0.0
Rear CW stringers	2	5.8	27.9	324	0.00	0.0
Rear CW grating	1	3	51.9	156	0.00	0.0
Point Walkaround	0.5	130	1	65	5.00	0.3
Vee Walkaround	0	91	1	0	7.50	0.0
Handrails	1	8	16.5	132	0.00	0.0
Lights	0	50	1	0	9.09	0.0
				3654		13.9

**Side 2**

	Number	Load	Area/Length	Total	Loc.	Mom.
Face	1	3	294	882	4.25	3.7
Stringers	3	5.8	24.5	426	3.41	1.5
Clips	6	6.6	0.33	13	3.41	0.0
Uprights	2	9	12.75	230	3.00	0.7
Hangrail/lat brace	1	4.9	24.5	120	3.00	0.4
Front CW ledgers	2	6.7	5.70	76	6.09	0.5
Ledger Clips	4	4.9	0.42	8	3.00	0.0
Front CW stringers	2	5.8	34.17	396	6.09	2.4
Front CW grating	1	3	87.2	262	6.09	1.6
Apron	0	3	6.125	0	3.00	0.0
Rear CW stringers	0	5.8	27.9	0	1.75	0.0
Rear CW grating	0	3	51.9	0	1.75	0.0
Point Walkaround	0.5	130	1	65	5.00	0.3
Vee Walkaround	0	91	1	0	7.50	0.0
Handrails	1	8	16.5	132	1.75	0.2
Lights	1	50	1	50	9.09	0.5
				2661		11.8

**Common**

	Number	Load	Area/Length	Total	Loc.	Mom.
Upper Spreaders	2	9	5.51	99	0.00	0.0
End Plates	4	8	0.33	11	0.00	0.0
Lower Spreaders	2	16	5.51	176	0.00	0.0
End Plates	4	6.8	1.00	27	0.00	0.0
Moonbeams	0	16	0.00	0	0.00	0.0
Torsion Pipe	1	27.8	18	500	0.00	0.0
Ladders	1	8	12.75	102	0.00	0.0
X-bracing	4	1.5	18.78	113	0.00	0.0
Bolts	1	200	1	200	0.00	0.0
Safety system	3	50	1	150	0.00	0.0
Head Plate	0	61	4.34	0	0.00	0.0
Connection Beams	2	19.0	2.08	79	0.00	0.0
Box Plates	0	30.6	1.66	0	0.00	0.0
Gussets1	0	0.21	31.25	0	0.00	0.0
Gussets2	0	0.21	102.19	0	0.00	0.0
Misc	1	1000	1	1000	0.00	0.0
				2457		

Total Weight	8772	Net Moment (abs)	2.071492
Total Weight without faces	6014	Net Offset	0.236153



CLIENT CLEAR CHANNEL  
 VOSS NO. 23-017-574  
 JOB 25-3786  
 DATE 3/28/2024 ENG. WY

9/16

**Detailed Deadload Takeoff**

**Two Heavy Faces**

**Side 1**

	Number	Load	Area/Length	Total	Loc.	Mom.
Face	1	8	234.465	1876	4.25	8.0
Stringers	0	5.8	24.5	0	3.41	0.0
Clips	2	6.6	0.75	10	3.41	0.0
Uprights	2	9	12.75	230	3.00	0.7
Hangrail/lat brace	1	4.9	24.5	120	3.00	0.4
Front CW ledgers	2	6.7	5.70	76	6.09	0.5
Ledger Clips	4	4.9	0.42	8	3.00	0.0
Front CW stringers	2	5.8	34.17	396	6.09	2.4
Front CW grating	1	3	87.2	262	6.09	1.6
Apron	0	3	6.125	0	3.00	0.0
Rear CW stringers	2	5.8	27.9	324	0.00	0.0
Rear CW grating	1	3	51.9	156	0.00	0.0
Point Walkaround	0.5	130	1	65	5.00	0.3
Vee Walkaround	0	91	1	0	7.50	0.0
Handrails	1	8	16.5	132	0.00	0.0
Lights	0	50	1	0	9.09	0.0
				3654		13.9

**Side 2**

	Number	Load	Area/Length	Total	Loc.	Mom.
Face	1	8	234.465	1876	4.25	8.0
Stringers	0	5.8	24.5	0	3.41	0.0
Clips	2	6.6	0.75	10	3.41	0.0
Uprights	2	9	12.75	230	3.00	0.7
Hangrail/lat brace	1	4.9	24.5	120	3.00	0.4
Front CW ledgers	2	6.7	5.70	76	6.09	0.5
Ledger Clips	4	4.9	0.42	8	3.00	0.0
Front CW stringers	2	5.8	34.17	396	6.09	2.4
Front CW grating	1	3	87.2	262	6.09	1.6
Apron	0	3	6.125	0	3.00	0.0
Rear CW stringers	0	5.8	27.9	0	1.75	0.0
Rear CW grating	0	3	51.9	0	1.75	0.0
Point Walkaround	0.5	130	1	65	5.00	0.3
Vee Walkaround	0	91	1	0	7.50	0.0
Handrails	1	8	16.5	132	1.75	0.2
Lights	0	50	1	0	9.09	0.0
				3175		14.1

**Common**

	Number	Load	Area/Length	Total	Loc.	Mom.
Upper Spreaders	2	9	5.51	99	0.00	0.0
End Plates	4	8	0.33	11	0.00	0.0
Lower Spreaders	2	16	5.51	176	0.00	0.0
End Plates	4	6.8	1.00	27	0.00	0.0
Moonbeams	0	16	0.00	0	0.00	0.0
Torsion Pipe	1	27.8	18	500	0.00	0.0
Ladders	1	8	12.75	102	0.00	0.0
X-bracing	4	1.5	18.78	113	0.00	0.0
Bolts	1	200	1	200	0.00	0.0
Safety system	3	50	1	150	0.00	0.0
Head Plate	0	61	4.33	0	0.00	0.0
Connection Beams	2	19.0	2.08	79	0.00	0.0
Box Plates	0	30.6	1.65	0	0.00	0.0
Gussets1	0	0.21	31.25	0	0.00	0.0
Gussets2	0	0.21	102.19	0	0.00	0.0
Misc	1	1000	1	1000	0.00	0.0
				2457		

Total Weight 9286 Net Moment (abs) 0.23155  
 Total Weight without faces 5535 Net Offset 0.024936

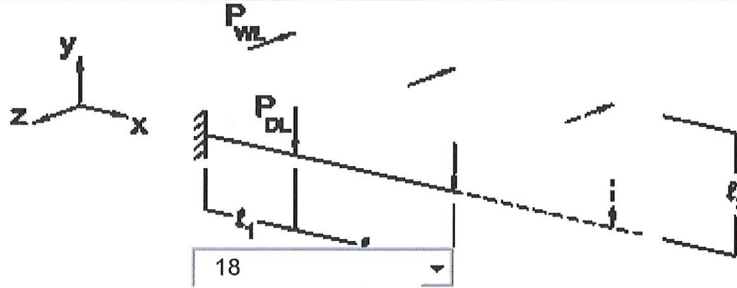


CLIENT CLEAR CHANNEL  
 VOSS NO. 23-017-574  
 JOB 25-3786  
 DATE 3/28/2024 ENG. WY

10/16

**Torsion Pipe**

Pr -0.058 kips (axial)  
 Mrx 33.593 ft-kips (torsion)  
 Mry 41.399 ft-kips (WL)  
 Mrz 45.669 ft-kips (DL)  
 Mrs 61.64037 ft-kips  
 Vres 7.934681 kips



IC Gov **3.213946**

LC 5  
 Member M42  
 Section 2

**Pipe Properties**

E (ksi)	Fy (ksi)	Diameter D (in)	Ins. Diam. D <sub>1</sub> (in)	Wall thickness t (in)	t <sub>eff</sub> (in)	D/t	rad. of gyr. r (in)	Weight (lb/ft)
29000	35	8.625	8.04375	0.3125	0.290625	29.68	2.95	27.77
Area A (in <sup>2</sup> )	I (ksi)	S (in <sup>3</sup> )	Z (in <sup>3</sup> )	J (in <sup>4</sup> )	C (in <sup>3</sup> )	Bending Compact?	Axial Compact?	
7.61	66.2	15.3	20.2	132.3	30.7	Compact	Compact	
λ <sub>p</sub> bending	58.00	λ <sub>r</sub> bending	256.86					
λ <sub>p</sub> axial	-	λ <sub>r</sub> axial	91.14					

**Axial Checks**

r <sub>eff</sub> from above (in)	Length above (for r) (ft)	Length of this pipe (ft)	Total Length (ft)	r <sub>eff</sub> (in)	K	Kl/r	Fe (ksi)
2.95	0	9	9	2.94842593	2.1	76.9224004	48.371782
Ω <sub>c</sub>	1.67						

**Flexural buckling Limit State**

Q=Qa ?? Q=1.0  
 F<sub>cr</sub> -35 ksi Ft -20.958084 ksi P<sub>n</sub>/Ω<sub>c</sub> = -159.4805 kips

**Flexure**

Ω<sub>b</sub> 1.67 D/t max 372.857143  
 Applicable Limit States: Yielding,  
 Yielding "Fb" = 27.592814 ksi (= Fy/Ω<sub>b</sub>\*Z/C) M<sub>n</sub>/Ω<sub>b</sub> = 35.271617 ft-kips

**Local Buckling**

"Fb" =

**Torsion and Shear**

**Shear yielding and shear buckling**

Ω<sub>v</sub> 1.67  
 F<sub>cr</sub>/Ω<sub>v</sub> = "Fv" = 12.5748503 V<sub>c</sub> = V<sub>n</sub>/Ω<sub>v</sub> 47.84414 kips

**Torsion**

Ω<sub>T</sub> 1.67  
 F<sub>cr</sub>/Ω<sub>T</sub> = "Fv<sub>T</sub>" = 12.5748503 T<sub>c</sub> = T<sub>n</sub>/Ω<sub>T</sub> 32.14836 ft-kips

Torsion pipe is overstressed without reinforcement. Provide reinforcement per following pages.

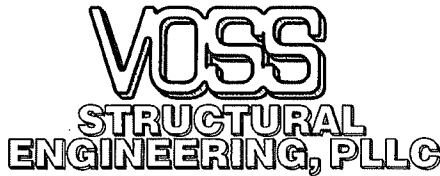
**Identity Checks**

H2: Pr/Pc 0.000364 Use H2-1 Axial Tension H3: Tr/Tc 1.04493674 Use checks Below

IC = 1.747955

IC = 3.21394582

**DON'T USE 8.6" diam x 0.313" thick, Fy = 35 ksi**



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CLIENT CLEAR CHANNEL

VOSS NO. 23-017-574

JOB 25-3786

DATE 28 MAR 2024

ENG. WY

11/16

p.1 of 3

TORSION PIPE REINFORCEMENT

Check channel reinforced torsion pipe with  $F_y = 50$  ksi channels (T.P.  $F_y = 35$  ksi)

Pipe alone:  $\frac{M_n}{\Omega} = 35.27$  k-ft

Try MCB x 22.8 channels → check for compactness:

$b = 8 - 2(0.525) = 6.95$  in. }  $b/t_c = \frac{6.95}{0.427} = 16.28$

$t = t_w = 0.427$  in.

From table B4.1b in AISC 15,

for flange cover plates:  $\lambda_p = 1.12 \sqrt{\frac{E}{F_y}}$   
 $\lambda_p = 1.12 \sqrt{\frac{29000}{50}} = 26.97$

$26.97 > 16.28 \therefore$  MCB x 22.8 is compact

Channels alone:

$\frac{M_n}{\Omega} = \frac{F_y \cdot Z_{eff}}{\Omega}$  where  $Z_{eff} = 2(6.7) \cdot 3.66$  in<sup>3</sup> = 49.04 in<sup>3</sup>

$= \frac{50 \cdot 49.04}{1.67} = 1468.38$  k-in OR 122.37 k-ft

$Z_{eff} = 20.2 + 49.04 = 70$  in<sup>3</sup>

Use pipe req'd strength for torsion & axial loads

$IC = \left(\frac{P_r}{P_c} + \frac{M_r}{M_c}\right) + \left(\frac{V_r}{V_c} + \frac{T_r}{T_c}\right)^2 \leq 1.0$

$\therefore IC_{CHANNEL} = \frac{0.724}{325} + \frac{75.76}{(35.27 + 122.37)} + \left(\frac{6.79}{132} + \frac{28.09}{45}\right)^2$

$IC_{CHANNEL} = 0.939 \therefore$  O.K.

For torsion pipe:  $f_b = \frac{M \cdot c}{I_{yos}} = \frac{75.76 \text{ k-ft} \cdot 12 \text{ in/ft} \cdot 8.625 \text{ in}/2}{282 \text{ in}^4} = 13.90$  ksi

$F_b = 27.59$  ksi

$IC_{TP} = \frac{0.724}{325} + \frac{13.90}{27.59} + \left(\frac{6.79}{132} + \frac{28.09}{45}\right)^2 = 0.963 \therefore$  O.K.

USE MCB x 22.8 CHANNELS @  $F_y = 50$  ksi TO REINFORCE EXISTING 8" STD PIPE w/ reinforcement, pipe meets new code

CHECK W/ RISA ANALYSIS RESULTS

LCS, TOR 2 (between corr beams)

$Z = 2(6.7) \cdot 2.75 = 36.85$  in<sup>3</sup>

$\frac{M_n}{\Omega} = \frac{50 \text{ ksi} \cdot 36.85 \text{ in}^3}{1.67} = 1103.3$  k-in OR 91.94 k-ft

$IC_{CHANNEL} = \frac{0.058}{440} + \frac{61.64}{35.27 + 91.94} + \left(\frac{7.93}{132} + \frac{33.59}{45}\right)^2$   
 $IC_{CHANNEL} = 1.13$

$IC_{pipe} : f_b = \frac{61.64 \cdot 12 \cdot 4.3125}{244} = 13.07$  ksi

USE MCB x 22.8 CHANNELS @  $F_y = 50$  ksi AS REINFORCEMENT

$IC_{pipe} = \frac{0.058}{440} + \frac{13.07}{27.59} + \left(\frac{7.93}{132} + \frac{33.59}{45}\right)^2 = 1.12$

↑  
Significantly Reduced





CLIENT: CLEAR CHANNEL  
 VOSS NO: 23-017-574  
 JOB: 25-3786  
 DATE: 3/28/2024 ENG. WY

12/16

**Steel Channel Reinforcement of Pipes**

**Pipe Properties**

Diameter	8.625 in	A	7.61 in <sup>2</sup>	J	132.3 in <sup>4</sup>
tnom	0.3125 in	I	66.2 in <sup>4</sup>	C	30.7 in <sup>3</sup>
tdes	0.291 in	S	15.3 in <sup>3</sup>	A <sub>0</sub>	54.56 in <sup>2</sup>
E	29000 ksi	Fy	42 ksi	D/t	27.6
λ <sub>p</sub> bending	48.33	λ <sub>r</sub> bending	214.05	λ <sub>p</sub> axial	-
λ <sub>p</sub> axial	-	λ <sub>r</sub> axial	-	λ <sub>r</sub> axial	75.95
Bending Compact?	Compact	Axial Compact?	Compact		

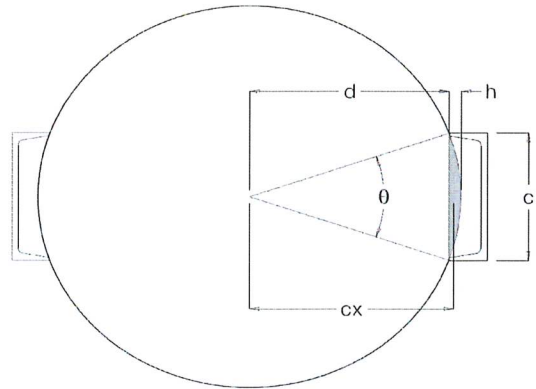
**Channel Properties**

MC8X22.8

A	6.7 in <sup>2</sup>	d	8 in	tw	0.427 in
I <sub>x</sub>	63.8 in <sup>4</sup>	bf	3.5 in	tf	0.525 in
I <sub>y</sub>	7.01 in <sup>4</sup>	x	1.01 in		

**Circular Segment properties at intersection of channel**

c	8 in	θ <sub>channel</sub>	2.38 rad
d	1.61 in	h	2.70 in
C <sub>X</sub>	2.73 in	A <sub>segment</sub>	13.45783 in <sup>2</sup>



**Properties of Channel with respect to pipe**

C<sub>channel-x</sub> 4.10 in (max distance of CG)

**Loads acting on Pipe**

Pr	-0.058 kips	(axial)	
Mr <sub>x</sub>	33.593 ft-kips	(torsion)	
M <sub>r<sub>y</sub></sub>	41.399 ft-kips		
M <sub>r<sub>z</sub></sub>	45.669 ft-kips		
M <sub>res</sub>	61.64037 ft-kips	α <sub>loads</sub>	0.834 rad (from y-axis)
V <sub>res</sub>	7.934681 kips		47.81 degrees (from y-axis)

**Full Composite Action**

**Pipe Allowables**

F <sub>a</sub>	-20.96 ksi	F <sub>b</sub>	27.59 ksi	F <sub>v</sub>	12.57 ksi
P <sub>c</sub>	-440 kips	V <sub>c</sub>	132 kips	T <sub>c</sub>	45 ft-kips
M <sub>c</sub>	88 ft-kips	T/T <sub>c</sub>	0.751	<b>IC</b>	<b>1.360</b>
		I <sub>c<sub>no tors</sub></sub>	0.706	I <sub>c<sub>tors</sub></sub>	1.360

See previous pages for code check with 50ksi channels for the 35ksi pipe



CLIENT CLEAR CHANNEL  
 VOSS NO. 23-017-574  
 JOB 25-3786  
 DATE 3/28/2024 ENG. WY

13/16

**Channel Location Worksheet**

**Symmetrical Channel Locations**

Neutral axis is located at the center of the pipe

Number of channels

Description: 2 channels on z

r ≡ radius to centroid of channel

θ ≡ Angle from y-axis to centroid, rad

**Locations of channels with respect to local pipe axes:**

Channel	r	θ	A <sub>channel</sub>	y	z	I <sub>0Y</sub>	I <sub>0Z</sub>	I <sub>0YZ</sub>
1	4.10	1.57	6.7	0.00	4.10	7.0	63.8	0.0
2	4.10	4.71	6.7	0.00	-4.10	7.0	63.8	0.0

**Centroid of combined shape**

y' 0.00 in

z' 0.00 in

**Properties of combined shape with respect to local pipe axes and centroid of combined shape**

A	21.01 in <sup>2</sup>	I <sub>ZCG</sub>	194 in <sup>4</sup>	A <sub>0</sub>	73.4 in <sup>2</sup>
I <sub>ZCG</sub>	0 in <sup>4</sup>	I <sub>YCG</sub>	306 in <sup>4</sup>		

**Locations of channels with respect to Mres:**

Channel	r	θ	A <sub>channel</sub>	y	z	I <sub>0Y</sub>	I <sub>0Z</sub>	I <sub>0YZ</sub>
1	4.10	2.41	6.7	-3.04	2.75	38.2	32.6	28.3
2	4.10	5.55	6.7	3.04	-2.75	38.2	32.6	28.3

**Centroid of combined shape**

y' 0.00 in

z' 0.00 in

**Properties of combined shape with respect to local pipe axes and centroid of combined shape**

A	21.01 in <sup>2</sup>	I <sub>ZCG</sub>	255 in <sup>4</sup>	A <sub>0</sub>	73.4 in <sup>2</sup>
I <sub>ZCG</sub>	-56 in <sup>4</sup>	I <sub>YCG</sub>	244 in <sup>4</sup>		

**Finding maximum distances from Mres axis**

Channel	θ <sub>top</sub>	θ <sub>bot</sub>	y <sub>top</sub>	z <sub>top</sub>	y <sub>bot</sub>	z <sub>bot</sub>
1		3.59	1.217432	-6.47373	0.469567	-1.10076
2		6.73	4.359024	6.473734	-0.46957	1.100762

I<sub>add</sub>  
Z<sub>eff</sub>  
J<sub>eff</sub>

**Section Properties of Combined Shape**

S<sub>y</sub> 38.2 in<sup>3</sup> S<sub>z</sub> 39.41406 in<sup>3</sup>



CLIENT CLEAR CHANNEL  
 VOSS NO. 23-017-574  
 JOB 25-3786  
 DATE 3/28/2024 ENG. WY

14/16

**Channel Welding Worksheet**

8.625" x 0.3125" with 2 - MC8X22.8 Channels

**Loads due to bending**

Q 20.4 in<sup>3</sup> I<sub>net</sub> 244 in<sup>4</sup>  
 V<sub>res</sub> 7.93 kips q<sub>b</sub> 0.66 k/in total  
 each weld: q<sub>b</sub>  k/in each weld

**Loads due to torsion**

M<sub>tors</sub> 33.59 ft-kips q<sub>t</sub>  k/in each weld  
 A<sub>o</sub> 73.42 in<sup>2</sup>

**Total loads on intermittant welds:**

q<sub>tot</sub>  k/in total

Weld size  in fillet  
 Weld spacing  in o.c.  
 Length req'd  in long

**Use 0.3125" welds, 5.5" long, 8" o.c.**

**End Welds:**

M<sub>tors</sub> 62 ft-kips  
 T Max 61.7 kips/channel q<sub>t</sub> 2.75 k/in each weld

Weld size  in fillet  
 Weld Length  in  
 Weld size req'd  in long 0.94 Accept

**Use 0.3125" Fillet welds, 19" long at each end**

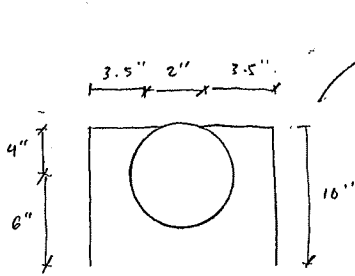


7264 W Benton Dr, Frankfort, IL 60423  
(815) 595-VOSS (8677)

CLIENT CLEAR CHANNEL OUTDOOR  
VOSS NO. 23-017-574  
JOB 25-3786  
DATE 28 MAR 2024 ENG. WY **15/16**

p. 2 of 3

WELD @ CONNECTION BEAMS



$b = 9''$   
 $d = 10''$   
TWISTING  $\rightarrow M_{rx} \text{ (torsion)} = 33.59 \text{ ft}\cdot\text{k}$

$$J_w = \frac{(b+2d)^3}{12} - \frac{d^2(b+d)}{b+2d}$$

$$J_w = \frac{(9+20)^3}{12} - \frac{10^2(9+10)}{29}$$

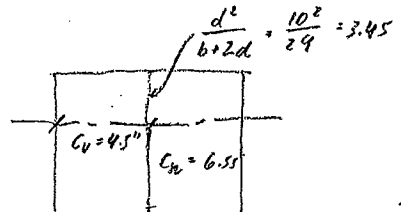
$$J_w = 787.59 \text{ in}^3$$

$$f_H = \frac{33.59 \text{ ft}\cdot\text{k} \cdot 12 \cdot 6.55 \text{ in}}{787.59 \text{ in}^3} = 3.35 \text{ k/in}$$

$$f_V = \frac{33.59 \text{ ft}\cdot\text{k} \cdot 12 \cdot 4.5 \text{ in}}{787.59 \text{ in}^3} = 2.303 \text{ k/in}$$

$$f_r = \sqrt{f_H^2 + (f_V + f_{SV})^2}$$

$$f_r = 4.23 \text{ k/in}$$



BENDING from sheet  
 $f = \frac{M_x}{S_w}$  where  $S_w = \frac{2bd+bd^2}{3}$   
 $S_w = 93.33$

$$f_{SV} = \frac{V}{A} = \frac{7.93 \text{ k}}{9+2(10) \text{ in}} = 0.273 \text{ k/in}$$

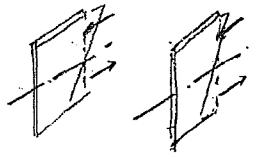
$$f = \frac{45.67 \text{ ft}\cdot\text{k} \cdot 12 \text{ in/ft}}{93.33 \text{ in}^2}$$

$$w = \frac{4.23 \text{ k/in}}{11.2 \text{ k/in}} = 0.377 \rightarrow \text{USE } \frac{7}{16}'' \text{ OR } \frac{1}{2}'' \text{ FILLET ALL AROUND}$$

$$f = 5.87 \text{ k/in} \rightarrow w = \frac{5.87}{11.2} = 0.524 \rightarrow \text{USE } \frac{9}{16}'' \text{ FILLET WELD ALL AROUND}$$

governs

SIZING OF PLATE



$M_x = 45.669 \text{ ft}\cdot\text{k}$   
 $F_y = 36 \text{ ksi}$

$C = T = \frac{45.669 \text{ ft}\cdot\text{k} \cdot 12 \text{ in/ft}}{2/3 \times 2}$

if  $F_y = 36 \text{ ksi}$  then

$$F_y = \frac{T}{A} = \frac{T}{t \cdot x}$$

$$36 \text{ ksi} = \frac{45.669 \text{ ft}\cdot\text{k} \cdot 12 \text{ in/ft}}{0.75 \times \frac{2}{3} \times 2}$$

$$x^2 = \frac{45.669 \cdot 12}{0.75 \cdot \frac{2}{3} \cdot 2 \cdot 36}$$

$$x^2 = 15.223 \rightarrow x = 3.9 \text{ in} \sim 4 \text{ in}$$

total wt of P is  $2x = 8''$

USE (2) 0.75" thick x 8" P  
in between conn. beams for  
transfer of loads.

# VOSS STRUCTURAL ENGINEERING, PLLC

7264 W Benton Dr, Frankfort, IL 60423  
(815) 595-VOSS (8677)

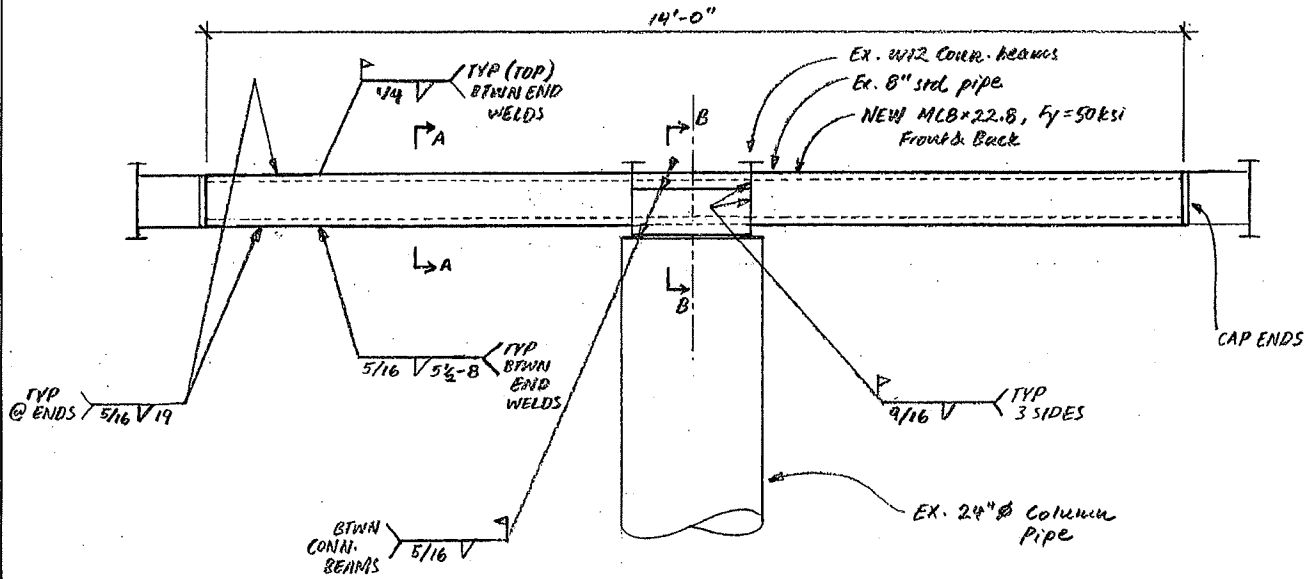
CLIENT CLEAR CHANNEL

VOSS NO. 23-017-574

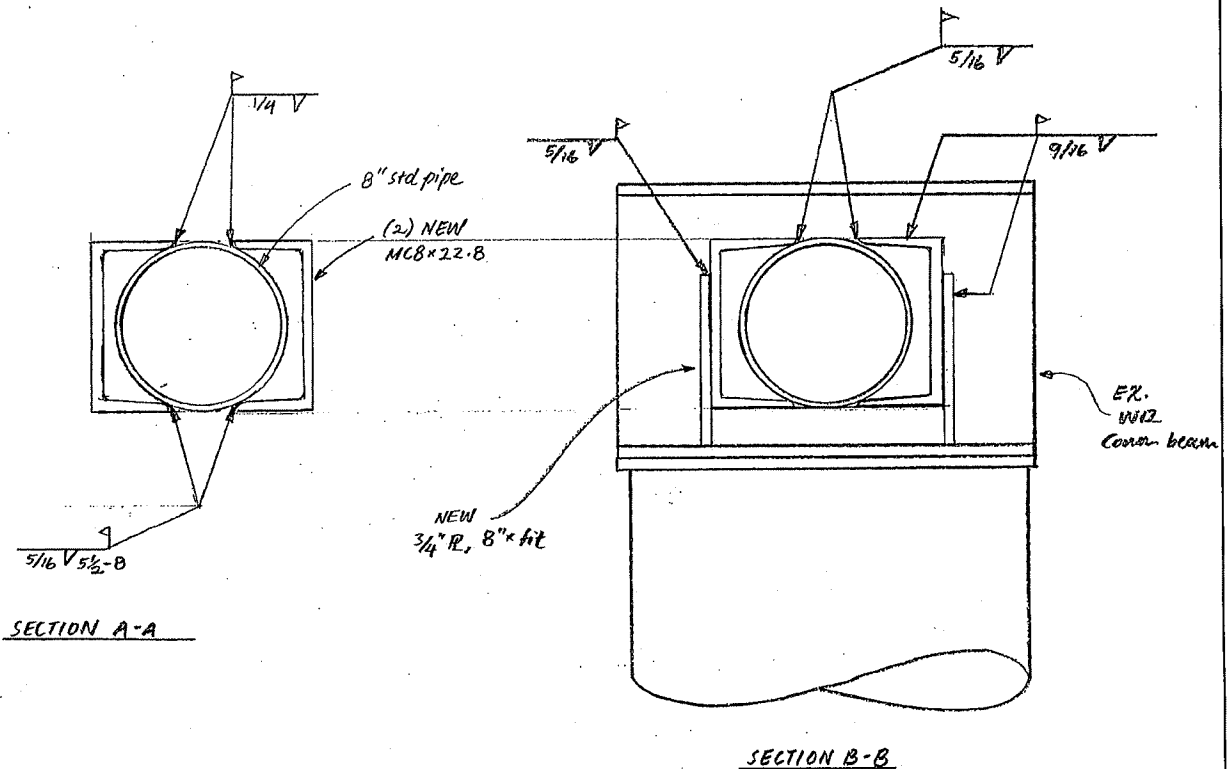
JOB 25-3786

DATE 28 MAR 2024 ENG. WY 16/16

p. 3 of 3



ELEVATION: TORSION PIPE REINFORCEMENT



September 21, 2023

Panel 5508

Nataliya Govdyak  
Real Estate Representative  
Clear Channel Outdoor  
4000 South Morgan St  
Chicago, IL 60609-2581

RE: P.I.N.# 07-36-401-003

Dear Ms. Govdyak,

In response to your inquiries:

- 1) That the above-described land parcel is currently located within the unincorporated limits of McHenry County.

*Yes, the parcel identified above is within the unincorporated limits of McHenry County.*

- 2) The current County zoning classification of the above-described land parcel.

*The parcel identified above is currently zoned I-1, Light Industrial District.*

Sincerely,

*Anna Kurtzman*

Anna B. Kurtzman, Senior Planner  
Planning & Zoning Department  
Office: 815-334-4560 | Direct: 815-334-4215 | [ABKurtzman@mchenrycountyil.gov](mailto:ABKurtzman@mchenrycountyil.gov)

**MCHENRY Co.**  
ILLINOIS



# McHENRY COUNTY

## ILLINOIS

### KEY INFO - Please Review

You can pay by electronic check, debit card, or credit card up until midnight on November 16, 2023. Cash or check payments can still be made in our office **IN PERSON** until 5pm November 17 at 2100 N. Seminary Avenue, Woodstock. Office hours are 7:30am to 5pm.

#### Property Information

<b>Parcel Number</b> 07-36-401-003	<b>Site Address</b> 500 MAGNET WAY WOODSTOCK, IL 60098	<b>Owner Name &amp; Address</b> JGA GLA LLC
<b>Tax Year</b> 2022 (Payable 2023) ▼		
<b>File Status</b> None		
<b>Property Class</b> 0080 - Industrial	<b>Tax Code</b> 07002 -	<b>Tax Status</b> Taxable
<b>Net Taxable Value</b> 43,216	<b>Tax Rate</b> 8.885091	<b>Total Tax</b> \$3,839.78 <span style="border: 1px solid black; padding: 2px;">Tax Bill</span>
<b>Township</b> HARTLAND TWP	<b>Acres</b> 0.0000	<b>Mailing Address</b> ARNOLD, JEFFREY P O BOX 1490 WOODSTOCK, IL, 60098-1490
<b>Legal Description</b> DOC 2007R0083528 (RE-RECORD) LT 3 ARNOLD SUB MEMO: RT 14 DEDICATED PER DOCS 368978 & 343730		

#### Assessments

Level	Homesite	Dwelling	Farm Land	Farm Building	Mineral	Total
DOR Equalized	43,216	0	0	0	0	43,216
Department of Revenue	43,216	0	0	0	0	43,216
Board of Review Equalized	43,216	0	0	0	0	43,216
Board of Review	43,216	0	0	0	0	43,216
S/A Equalized	43,216	0	0	0	0	43,216
Supervisor of Assessments	38,769	0	0	0	0	38,769
Township Assessor	38,769	0	0	0	0	38,769
Prior Year Equalized	38,769	0	0	0	0	38,769

There are 8 levels of assessments in an assessment year. The assessed value is not final for the year until all levels of assessment are complete. The assessment year is complete when the DOR Equalized line appears at the top of the list shown above.

#### Billing

Installment	Date Due	Tax Billed	Penalty Billed	Cost Billed	Drainage Billed	Total Billed	Amount Paid	Date Paid	Total Unpaid
1	06/12/2023	\$1,919.89	\$0.00	\$0.00	\$0.00	\$1,919.89	\$1,919.89	6/8/2023	\$0.00
2	09/12/2023	\$1,919.89	\$0.00	\$0.00	\$0.00	\$1,919.89	\$1,919.89	9/6/2023	\$0.00
<b>Total</b>		<b>\$3,839.78</b>	<b>\$0.00</b>	<b>\$0.00</b>	<b>\$0.00</b>	<b>\$3,839.78</b>	<b>\$3,839.78</b>		<b>\$0.00</b>

#### No Drainage / Special District Information

No Farmland Information

No Forfeiture Information

Parcel Genealogy

Relationship	Parcel Number	Action	Year	Change Effective Year	Completed
Parent Parcel	0736400021	N		2005	Yes

Parcel Owner Information

Name	Tax Bill	Address
JGA GLA LLC	N	

No Redemptions

No Sales History Information

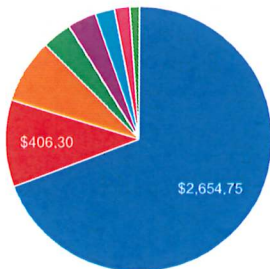
Payment History

Tax Year	Total Billed	Total Paid	Amount Unpaid
2022	\$3,839.78	\$3,839.78	\$0.00
2021	\$3,574.82	\$3,574.82	\$0.00
2020	\$3,578.88	\$3,578.88	\$0.00

Show 15 More

Taxing Bodies

District	Tax Rate	Extension
SCHOOL DIST 200	6.142990	\$2,654.75
WOODSTOCK FIRE RESCUE	0.940172	\$406.30
MCHENRY COUNTY	0.698158	\$301.73
HARTLAND TWP RD & BR	0.315449	\$136.32
COLLEGE DISTRICT 528 MCC	0.306028	\$132.25
MCHENRY CO CONSV	0.212478	\$91.82
HARTLAND TOWNSHIP	0.164981	\$71.30
RURAL WOODSTOCK LIBRARY	0.104835	\$45.31
<b>TOTAL</b>	<b>8.885091</b>	<b>\$3,839.78</b>



- SCHOOL DIST 200
- WOODSTOCK FIRE RESCUE
- MCHENRY COUNTY
- HARTLAND TWP RD & BR
- COLLEGE DISTRICT 528 MCC
- MCHENRY CO CONSV
- HARTLAND TOWNSHIP
- RURAL WOODSTOCK LIBRARY





**Make Check Payable to: McHENRY COUNTY COLLECTOR**  
**Remit payment to: P.O. Box 458, Crystal Lake, IL 60039-0458**  
*or pay on-line at: treasurer.mchenrycountyil.gov*

Parcel Number / PIN: **07-36-401-003**



**1st**  
**2022**

**\*\*DUPLICATE\*\***

ARNOLD JEFFREY  
P O BOX 1490  
WOODSTOCK IL 60098-1490

1ST INSTALLMENT FOR 2022	\$1,919.89
PENALTY	
INSTALLMENT AMOUNT PAID	\$1,919.89
INSTALLMENT BALANCE DUE DUE BY 06/12/2023	\$0.00

INCLUDE THIS COUPON WITH YOUR PAYMENT

16962

CHECK HERE IF CHANGING ADDRESS ON THE BACK

0736401003000000000014



Donna Kurtz - McHenry County Treasurer  
**Make Check Payable to: McHENRY COUNTY COLLECTOR**  
**Remit payment to: P.O. Box 458, Crystal Lake, IL 60039-0458**  
*or pay on-line at: treasurer.mchenrycountyil.gov*

Parcel Number / PIN: **07-36-401-003**



**2nd**  
**2022**

**\*\*DUPLICATE\*\***

ARNOLD JEFFREY  
P O BOX 1490  
WOODSTOCK IL 60098-1490

2ND INSTALLMENT FOR 2022	\$1,919.89
PENALTY	
INSTALLMENT AMOUNT PAID	\$1,919.89
INSTALLMENT BALANCE DUE DUE BY 09/12/2023	\$0.00

INCLUDE THIS COUPON WITH YOUR PAYMENT

0736401003000000000026

CHECK HERE IF CHANGING ADDRESS ON THE BACK

Taxing Body	Rate	Percent	Tax This Year	Tax Last Year
ENRY COUNTY	0.625255	7.04	\$270.22	\$255.03
ENRY COUNTY PENSION	0.072903	0.82	\$31.51	\$30.48
ENRY CO CONSV	0.212478	2.39	\$91.82	\$86.05
EGE DISTRICT 528 MCC	0.305922	3.44	\$132.20	\$127.77
EGE DISTRICT 528 MCC PENSION	0.000106	0.00	\$0.05	\$0.04
JOL DIST 200	5.883196	66.21	\$2,542.47	\$2,352.71
JOL DIST 200 PENSION	0.259794	2.92	\$112.28	\$109.46
DSTOCK FIRE RESCUE	0.778757	8.76	\$336.54	\$310.30
DSTOCK FIRE RESCUE PENSION	0.161415	1.82	\$69.76	\$61.20
L WOODSTOCK LIBRARY	0.104835	1.18	\$45.31	\$41.79
LAND TOWNSHIP	0.164981	1.86	\$71.30	\$70.71
LAND TWP RD & BR	0.315449	3.55	\$136.32	\$129.28

Totals 8.885091 \$3,839.78 \$3,574.82

**PARCEL NUMBER / PIN**

16962

**07-36-401-003**

**Late Payment Schedule**

	1ST	2ND
06/13 - 07/12	1,948.69	
07/13 - 08/12	1,977.49	
08/13 - 09/12	2,006.29	
09/13 - 10/12	2,035.08	1,948.69
10/13 - 11/12	2,063.88	1,987.49
11/13 - 11/17	2,092.68	2,016.29

**2022 Property Tax Bill**

**Assessed to:**  
JGA GLA LLC  
**Mail to:**  
ARNOLD JEFFREY  
P O BOX 1490  
WOODSTOCK IL 60098-1490

**Property location:**  
500 MAGNET WAY  
WOODSTOCK, IL 60098

**Legal Description:**  
DOC 2007R0083528 (RE-RECORD)  
LT 3  
ARNOLD SUB

MEMO: RT 14 DEDICATED  
PER DOCS 368978 & 343730

Fair Cash Value	129,660
S/A Value	38,769
S/A Multiplier	1.1147 X
S/A Equalized Value	43,216 =
Brd. of Review Value	43,216
Brd. of Review Multiplier	1.0000 X
Brd. of Review EQ Value	43,216 =
Home Improv./Vet Exemptions	0 -
State Multiplier	1.0000 X
State Equalized Value	43,216 =
Farmland and Bldgs. Value	0 +
Total Amt. Prior to Exemptions	43,216 =
Annual Homestead Exemptions	0 -
Sr. Freeze Abated Amount	0 -
Senior Homestead Exemption	0 -
Disabled Vet Homestead Ex	0 -
Disabled Person Exemption	0 -
Returning Veteran Exemption	0 -
Net Taxable Amount	43,216 =
Local Tax Rate	8.885091 X
Total Current Year Tax Due	\$3,839.78 =

FIRST PAYMENT RECEIVED	SECOND PAYMENT RECEIVED
1	2

Township	Tax Code	Property Class
HA	07002	0080
Sub Lot	Acres	Back Taxes
		NO
1st Installment	2nd Installment	
\$1,919.89	\$1,919.89	
Paid on	Paid on	
06/08/2023	09/06/2023	